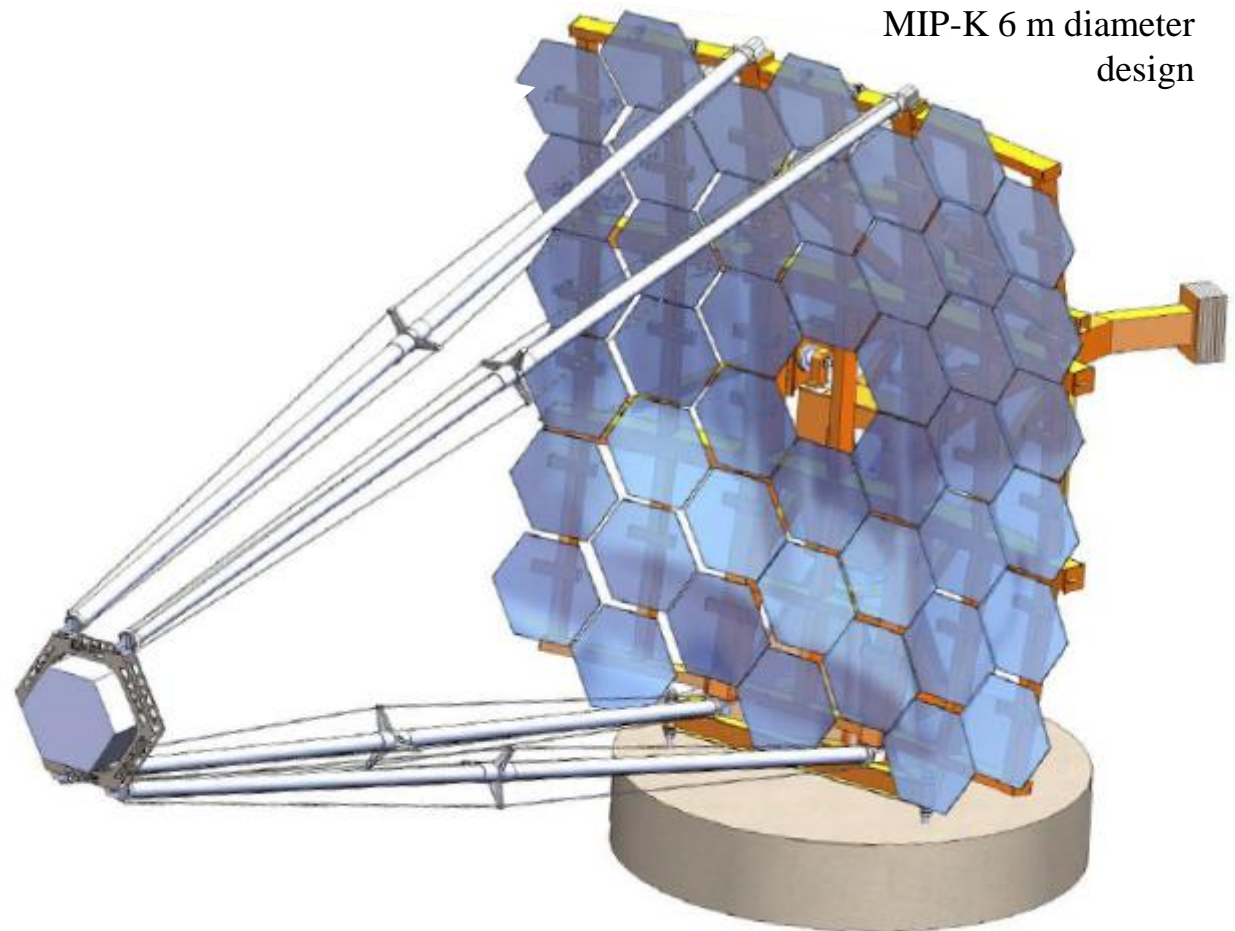


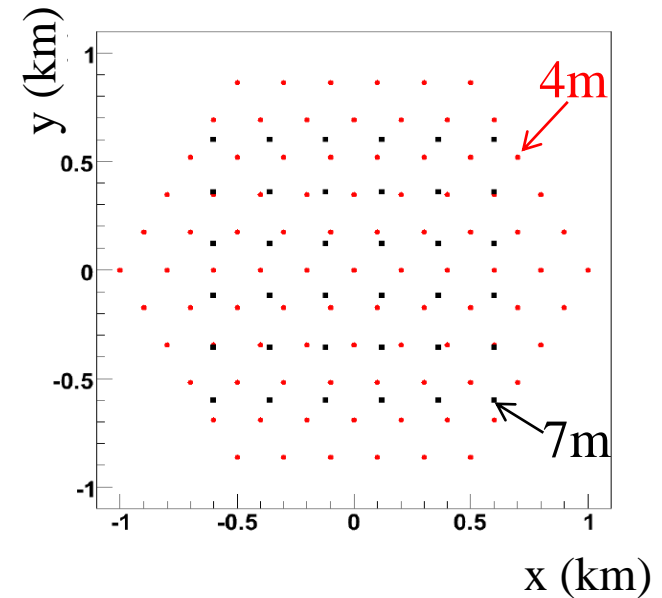
# Telescopes for the High Energy Section of the CTA

- Introduction
- Dual mirror telescope optics:
  - ◆ V17 parameters.
  - ◆ Light throughput.
  - ◆ PSFs and resolution.
  - ◆ Distortion and tolerances.
  - ◆ Flat camera elements.
  - ◆ Mirror shapes.
- Summary.

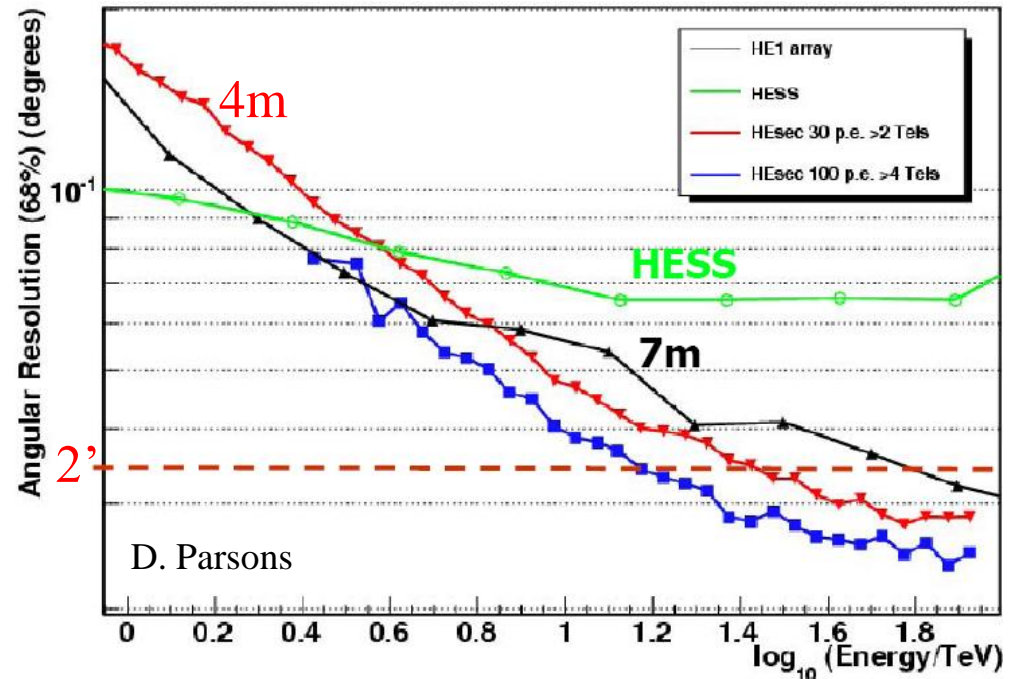


# Introduction

- Flux of highest energy photons small, need to cover large area.
- Two approaches possible:
  - ◆ Lots of cheap telescopes with moderate field of view separated by  $\sim 150$  m.
  - ◆ Fewer expensive telescopes with very large field of view allowing separations up to  $\sim 500$  m.
- Latter approach leads to smaller multiplicity, poorer angular resolution: use many small telescopes.
- Possibilities include:
  - ◆ D-C with  $\sim 7$  m diameter mirror.
  - ◆ Dual mirror, primary  $\sim 4$  m.



- Multiplicity and angular resolution.

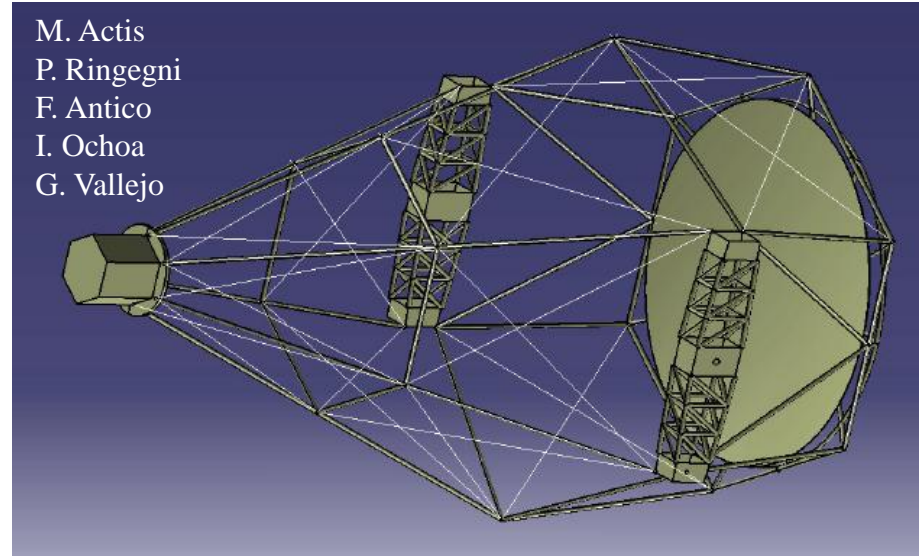


# Introduction

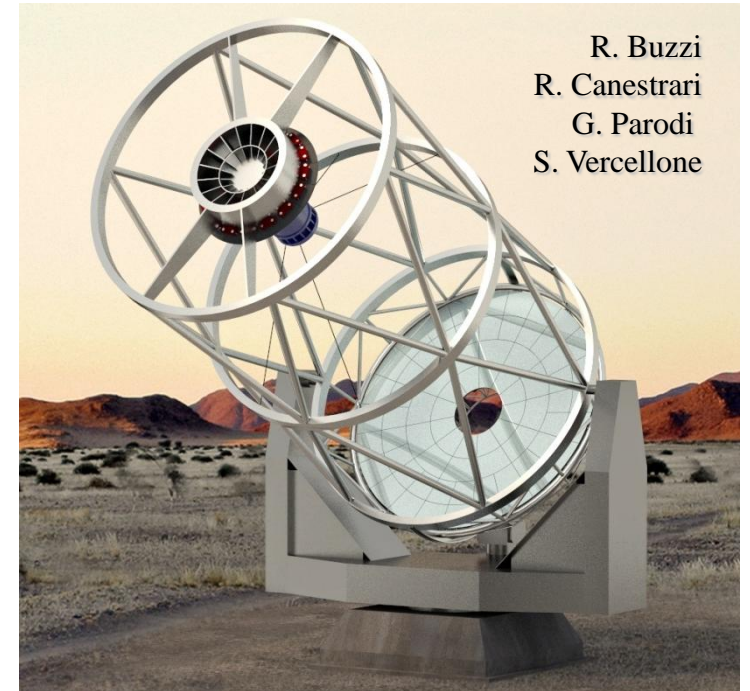
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- Typical requirements for telescopes:
  - ◆ Field of view of  $8\text{...}10^\circ$ .
  - ◆ Pixel size of around  $0.2\text{...}0.3^\circ$ .
- Davies-Cotton design,  $F \sim 12$  m, mirror diameter  $\sim 7$  m ( $F/D \sim 1.5$ ), pixels  $\sim 40$  mm, PM-based camera.
- Dual-mirror design,  $F \sim 2.3$  m, primary diameter  $\sim 4$  m ( $F/D \sim 0.6$ ), secondary diameter  $\sim 2$  m, pixels  $\sim 8$  mm, MAPM- or GAPD-based camera.
- Single mirror design using (solid) Winston Cones and GAPDs.
- Here describe progress with optical design of a dual mirror telescope.

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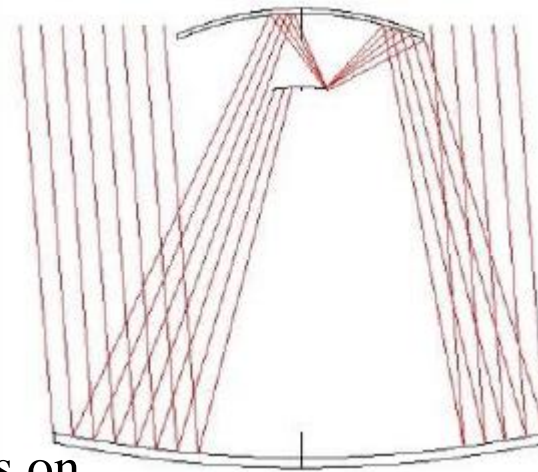
R. Buzzi  
R. Canestrari  
G. Parodi  
S. Vercellone



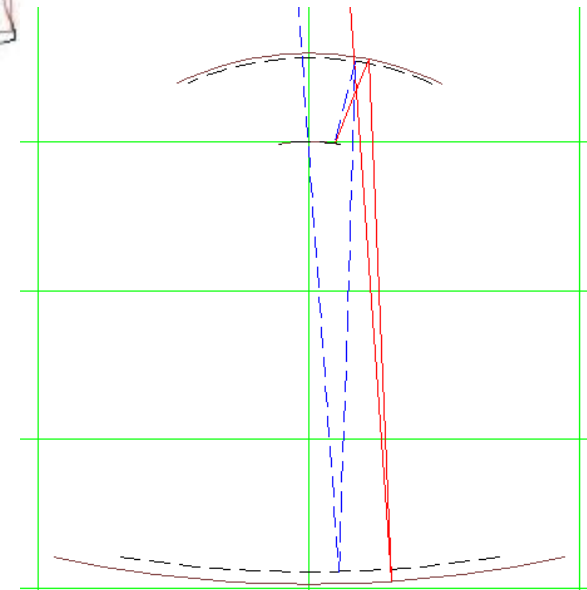
# Dual mirror optics

- Two optical design studies.
- Commercial package ZEMAX<sup>1</sup> (CfAI, Durham).
- “Exact Optics”<sup>2</sup> (Liverpool).
- Both approaches give PSFs consistent with pixel sizes of a few mm.
- Concern due to steep angle of rays on camera, particularly for “Exact Optics” solution, of up to 75°.
- Further optimisation (V11) using ZEMAX allowed reduction of max angle to below 60°.
- Results reported in Zeuthen.

- Ray tracing with  $\delta = 4.5^\circ$ :



J Schmoll



<sup>1</sup> <http://www.zemax.com/>

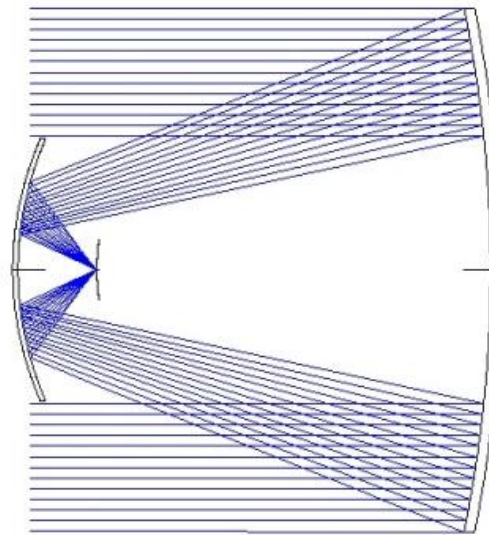
<sup>2</sup> Lynden-Bell, Mon. Not. R. Astron. Soc. **334**, 787-796 (2002).

# V17 parameters

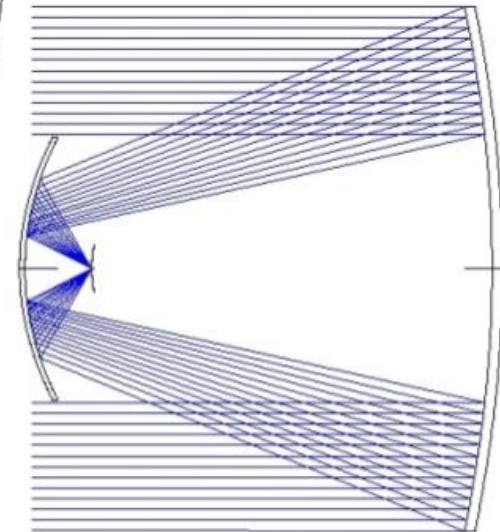
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- Further ZEMAX optimisation.
- In particular plate scale corrected and additional weight given to PSFs at large field angles in optimisation.
- Result (V17) is plate scale of 39.6 mm/° and increased uniformity of PSFs across field of view.
- Telescope parameters:
  - ◆  $F = 2.283$  m.
  - ◆  $D_p = 4$  m.
  - ◆  $D_s = 2$  m.
  - ◆  $D_{\text{cam}} = 0.36$  cm.
  - ◆ Dist. Prim. to Sec. 3.56 m.
  - ◆ Dist. Sec to Cam. 0.51 m.
  - ◆ Camera convex,  $\rho_{\text{cam}} = 1$  m.

- V13 (top) and V17 (bottom):

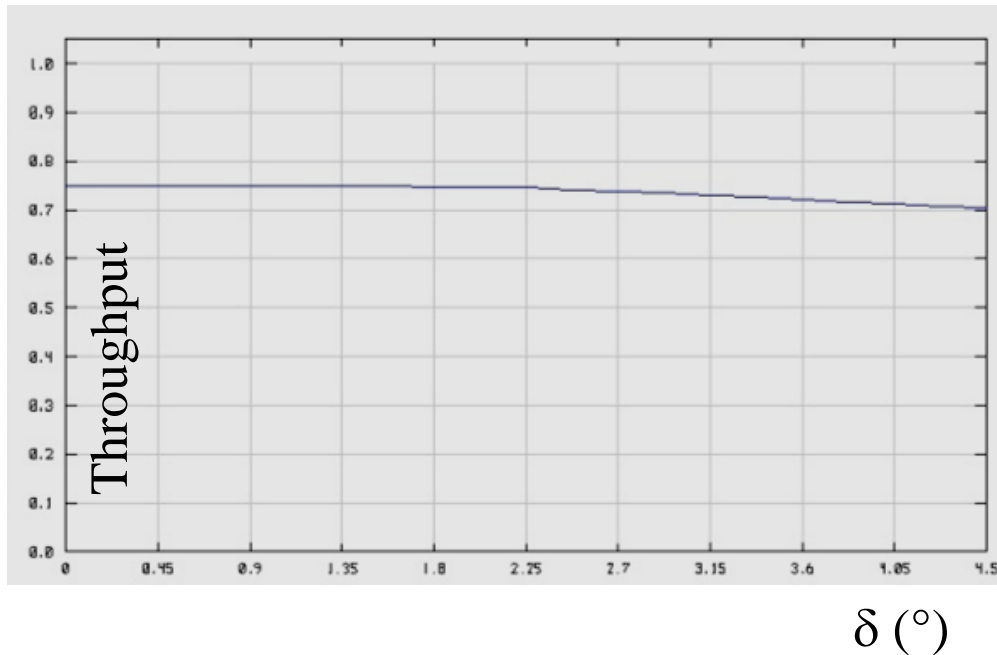


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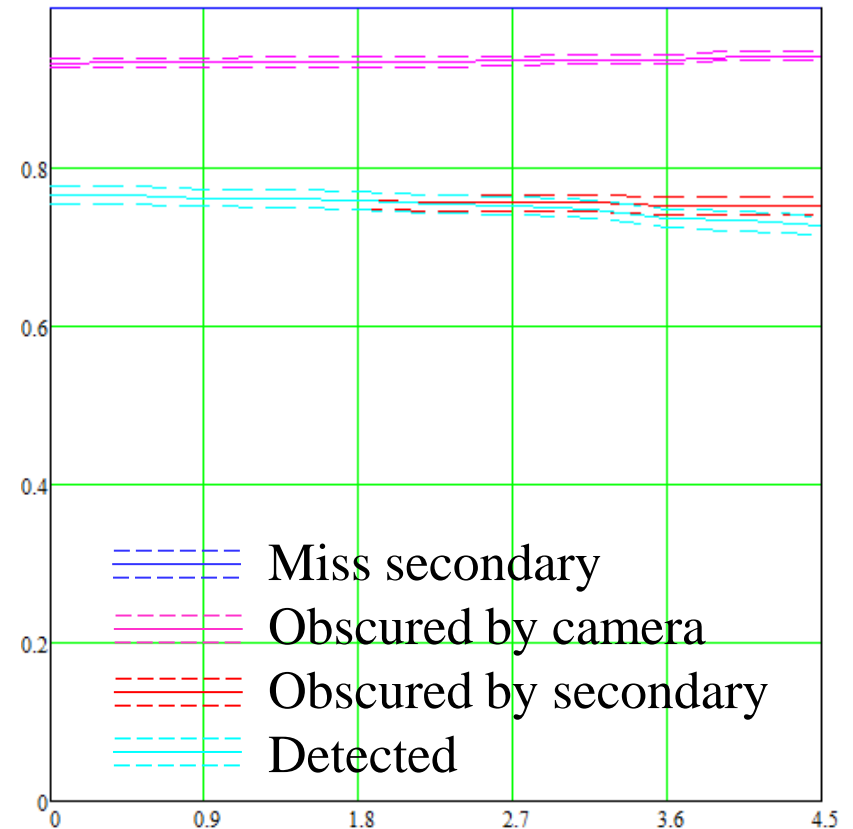
# Light throughput

- Geometrical throughput:



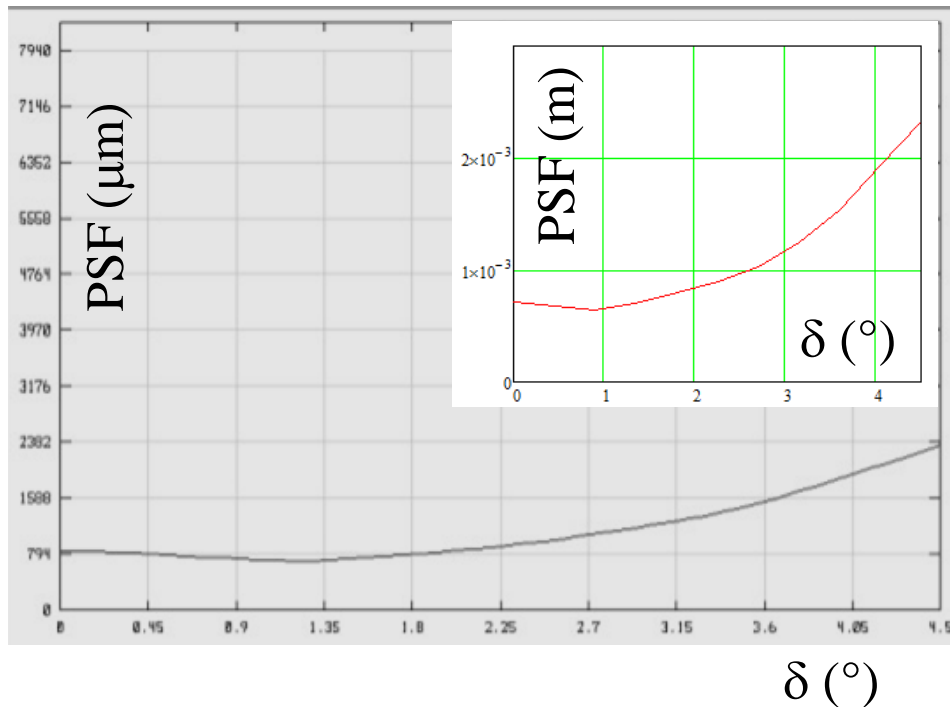
- Throughput varies from 75% to 71% (effective area 9.4 m<sup>2</sup> to 8.9 m<sup>2</sup>).

- Results independently checked.



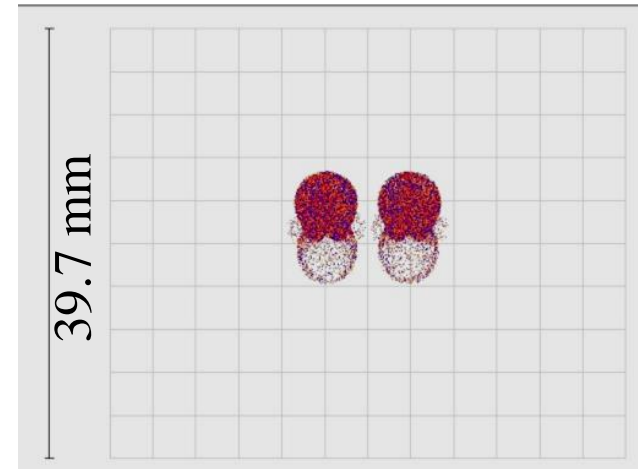
# PSFs and resolution

- PSFs (enclosed energy 70%):

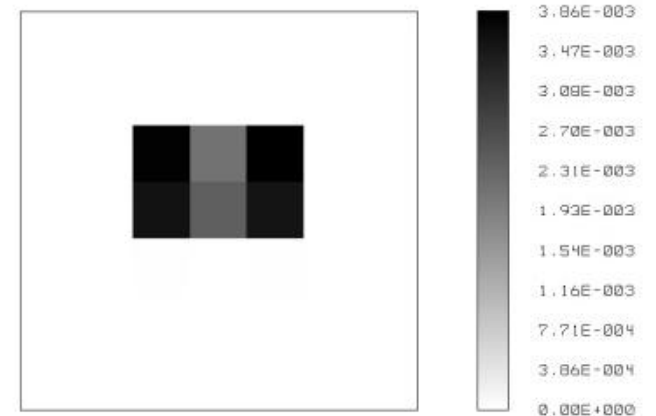


- 7940 mm = 0.2°.

- Resolution (images at 0.2° separation)...

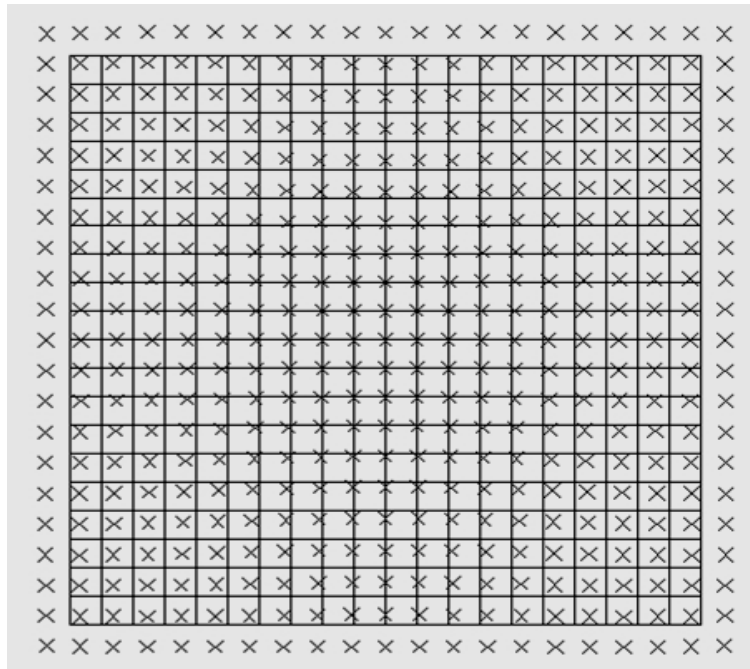


- ...dominated by pixel size (6.5 mm), not optical performance of telescope.



# Distortion and tolerances

## ■ Distortion:



- Maximum -2.5% at largest field angles.
- Isochronous.

## ■ Tolerances (monolithic mirrors):

Error	Surface	Tolerance
Distance deviation	M1 to M2	+/- 5 mm
	M2 to detector array	(+/- 5 mm) (*)
Surface irregularity	M1	20 $\mu\text{m}$ rms
	M2	50 $\mu\text{m}$ rms
Surface roughness	M1	1 $\mu\text{m}$ rms
	M2	1 $\mu\text{m}$ rms
Radius deviation	M1	+/- 10 mm
	M2	+/- 3 mm
	detector array	+/- 3 mm
Element decenter	M1	+/- 5 mm
	M2	+/- 5 mm
	detector array	+/- 5 mm
Element tilt	M1	+/- 0.14°
	M2	+/- 0.14°
	detector array	+/- 0.14°

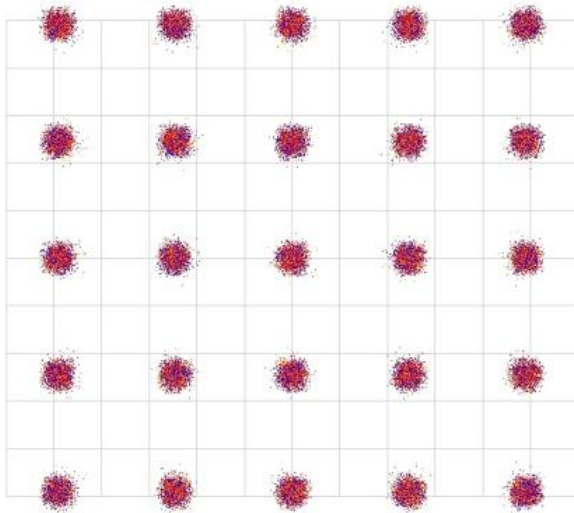
- Above modifications result in less than 10% increase in PSFs.
- Change of focus (M2 to camera) allowed as compensation, max 3.7 mm(\*).



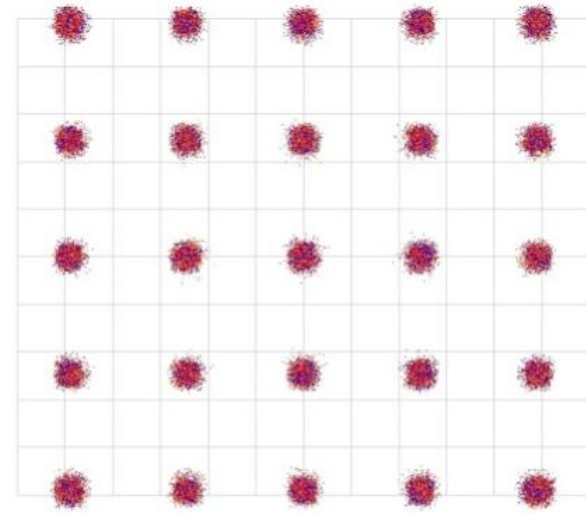
# Tolerances cont. and effect of flat camera elements

- Allowed error in position and angle of mirror segments (resulting in shift of image of less than 2.15 mm).

Element decentre	M1	$\pm 2$ mm
	M2	$\pm 2$ mm
Element tilt	M1	$\pm 0.17^\circ$
	M2	$\pm 0.5^\circ$
	Focal plane	$\pm 0.83^\circ$

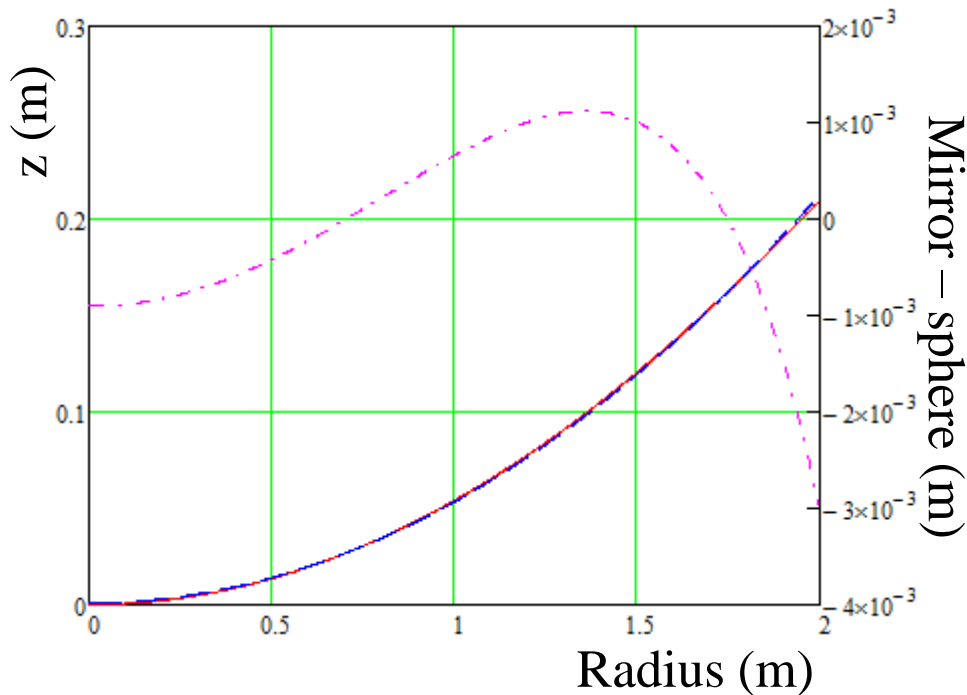


- Effects of constructing camera using flat tiles (e.g. of MAPMs) rather than curved surface investigated.
- Tile size  $52 \times 52$  mm<sup>2</sup>.
- No appreciable difference between images on curved (left) and flat (right) surfaces:

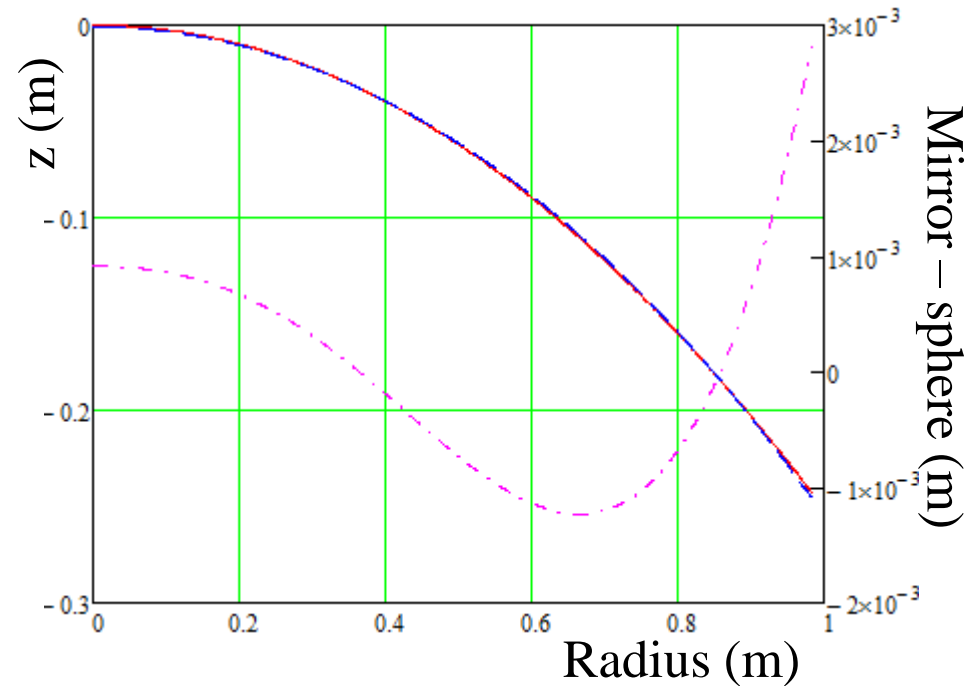


# Mirror shapes

- Mirrors aspherical, shape and deviation from closest sphere ( $R = 9.55$  m) for primary...



- ...and secondary ( $R = 2.10$  m).



# Summary

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- Optical design of dual mirror telescope has been further developed.
- PSFs (70% enclosed energy) below 2.5 mm ( $0.1^\circ$ ) achieved for field angles up to  $4.5^\circ$ .
- Geometrical throughput  $\sim 75\%$ : primary diameter 4 m implies effective area of around 9 m<sup>2</sup>.
- Tolerances reasonable.
- Investigation of mirror construction techniques required.
- Studies of sensors appropriate for camera needed.

